





FAME PRODUCTION FROM WASTE COOKING OIL THROUGH TRANSESTERIFICATION-OZONATION REACTION

- Generation of Gas-Liquid Flow in a Microchannel -

Aloisiyus Y. Widianto^{a,b}, Joelle Aubin^b, Martine Poux^b, and Catherine Xuereb^b ^aDepartment of Chemical Engineering-University of Surabaya, Jl. Raya Kalirungkut Surabaya-East Java, 60293 Indonesia ^bLaboratoire de Génie Chimique, Université du Toulouse, CNRS, Toulouse, France







BACKGROUND

- The scarcity of petroleum reserves will give the opportunity for renewable energy sources development
- A high percentage of FFA in WCO is a good opportunity for using it as raw material to produce biodiesel.
- The biodiesel stability is low due to high concentration of unsaturated ester. It can be improved by cracking double bond carbon chain (C=C)
- Transesterification-ozonolysis reaction involving three phases gas-



RESULTS

liquid-liquid will take place in microchannel. Therefore, a study of characteristic flow pattern in microchannels is needed.

OBJECTIVES

The study aims to find an intensified process technology for producing high-quality biodiesel involving double bond cracking in WCO to methyl esters, low energy consumption, process safety, high selectivity, and conversion. Therefore the purpose of this research is:

To find the characteristic flow pattern of gas-liquid in the microchannel by using air-methanol as a reference to carry out the transesterification-ozonolysis reaction in the microchannel.

MATERIALS & METHOD

Scheme of experimental equipment :



Range of air-methanol flow rate & dimensionless number:

- Methanol flow rate $(Q_L) = 0.06-2.8 \text{ ml/min}$
- Air flow rate $(Q_g) = 0.25 3.25 \text{ ml/min}$
- Reynolds number phase liquid $(Re_1) < 80$
- ρ = density μ = viscosity U = superficial



CONCLUSIONS

1. The observed flow patterns in the microchannel with ID = 1 mm,

Reynolds number phase gas (*Re_G*) < 7.5
 Capillary number (*Ca*) = 0.000025 - 0.0018

$$Re_{L} = \frac{\rho_{L}.U_{L}.d_{h}}{\mu_{L}} \qquad Re_{G} = \frac{\rho_{G}.U_{G}.d_{h}}{\mu_{G}} \qquad Ca = \frac{\mu_{L}.U_{L}}{\sigma}$$
$$d_{c} = 300; 530; 1000; 1500 \ \mu\text{m}; \ d_{g} = 500 \ \mu\text{m}$$
$$P_{gas inlet} = 1.2 \ bars$$

 $\sigma = surface$ c = surface c = liquidc = gas

c = channel

- 1.5 mm are Taylor and annular flow.
 The length of bubble increases with the increase in the ratio of superficial-gas velocity to superficial-liquid velocity.
 The length of bubbles in inlet and outlet section of the tube is different
- 4. The change of the length of the bubbles are due to the pressure drop along the tube and sometimes to coalescence phenomena

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